



POWER ELECTRONICS I

AC-DC Converters

Three-Phase Rectifiers

Dr. Islam Mohamed

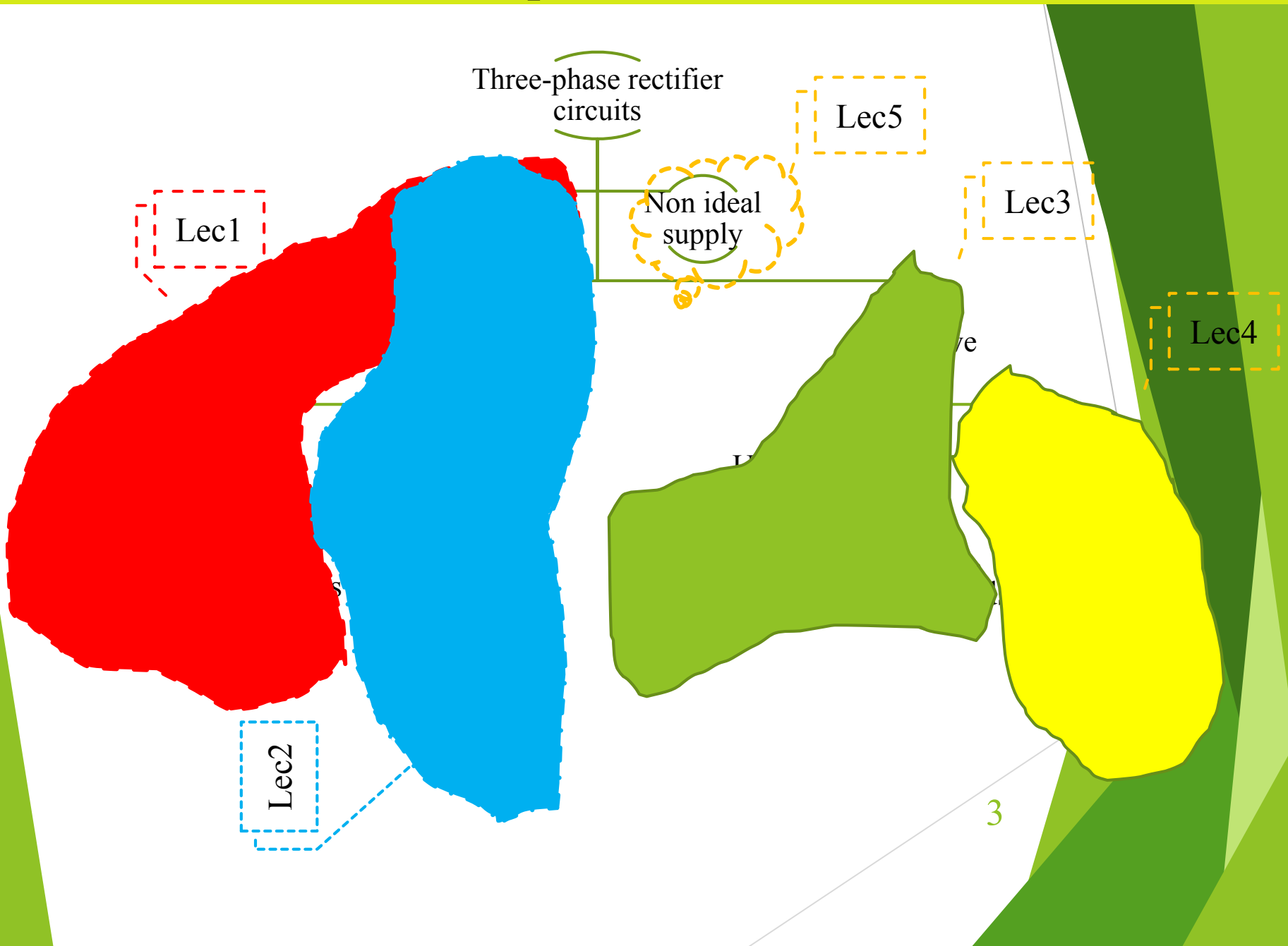
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Questions Lecture Four

- Q₁) what are the rating values of the Thyrisors in the converter?
- Q₂) Draw a relation between the rectification efficiency and firing angles for R-load and highly inductive loads.
- Q₃) Draw a relation between the average output voltage and firing angles for R-load and highly inductive loads.
- Q₄) Draw the load voltage and current waveforms if a freewheeling diode is connected incase RL-loads.
- Q₅) Draw the load voltage and current waveforms at for RL-loads if T2, T4, T6 are replaced with diodes At $\alpha = 30, 60, 90$

Three-phase rectifier Plan



Lecture three: Three-phase half-wave rectifiers with nonideal supply

Construction

- Circuit diagram
- Components

Operation

- Output waveforms with highly inductive load.

Analysis

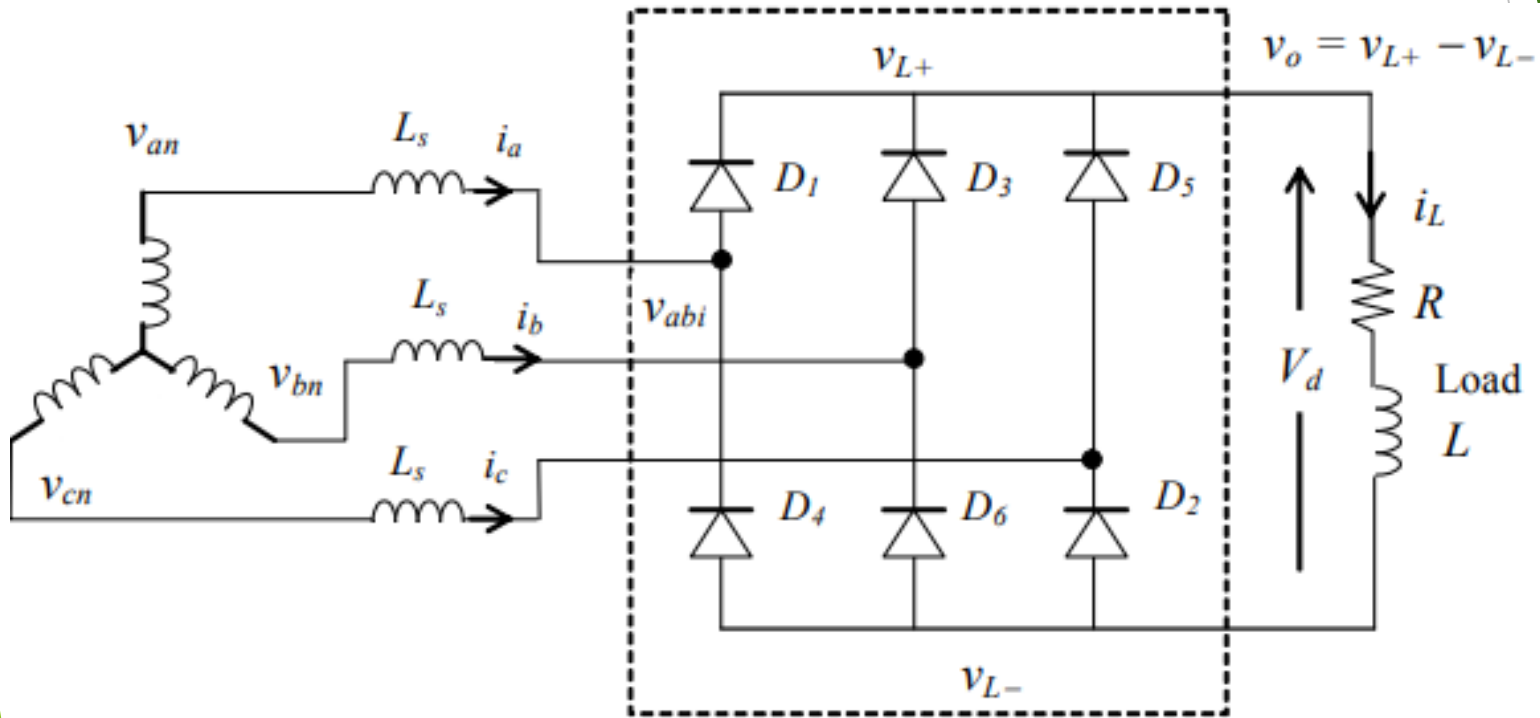
- Analysis of three-phase half wave controlled circuit
- Analysis of three-phase half wave uncontrolled circuit

End

- Summary
- Questions

Construction

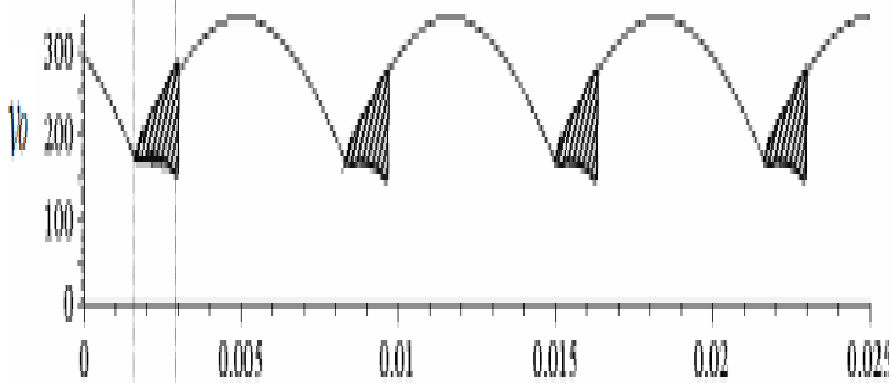
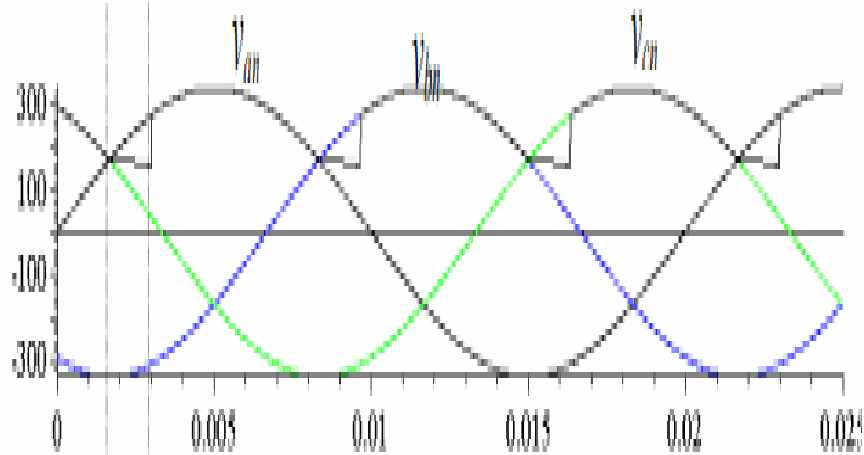
Power circuits and its components



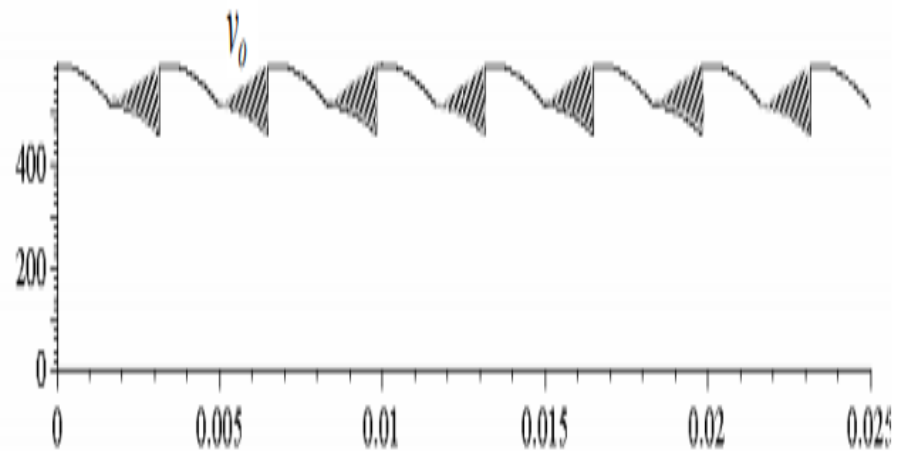
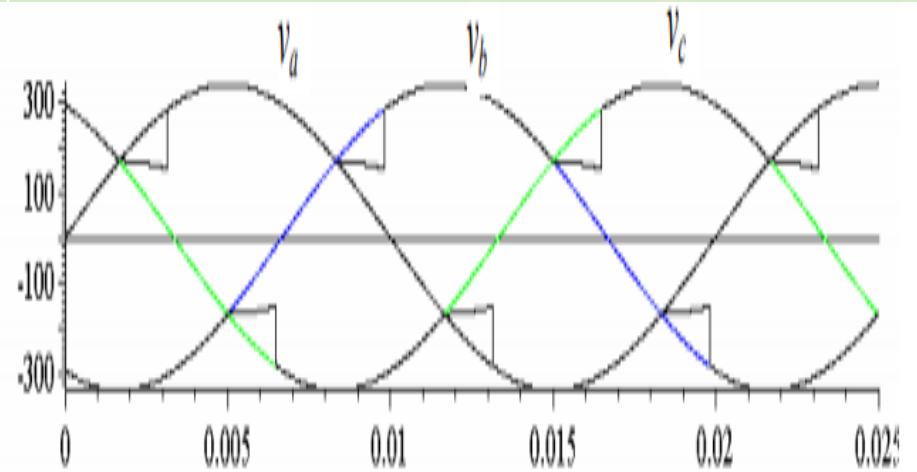
Operation

Output Voltage waveforms

Half-wave



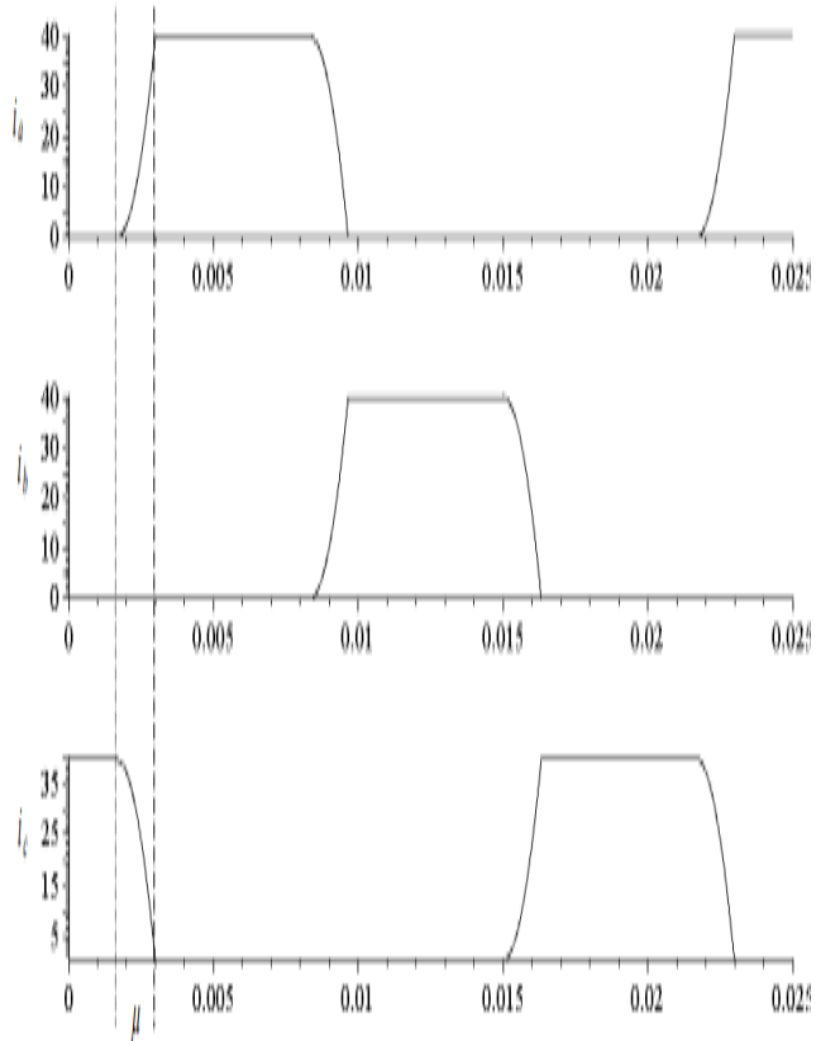
Full-wave



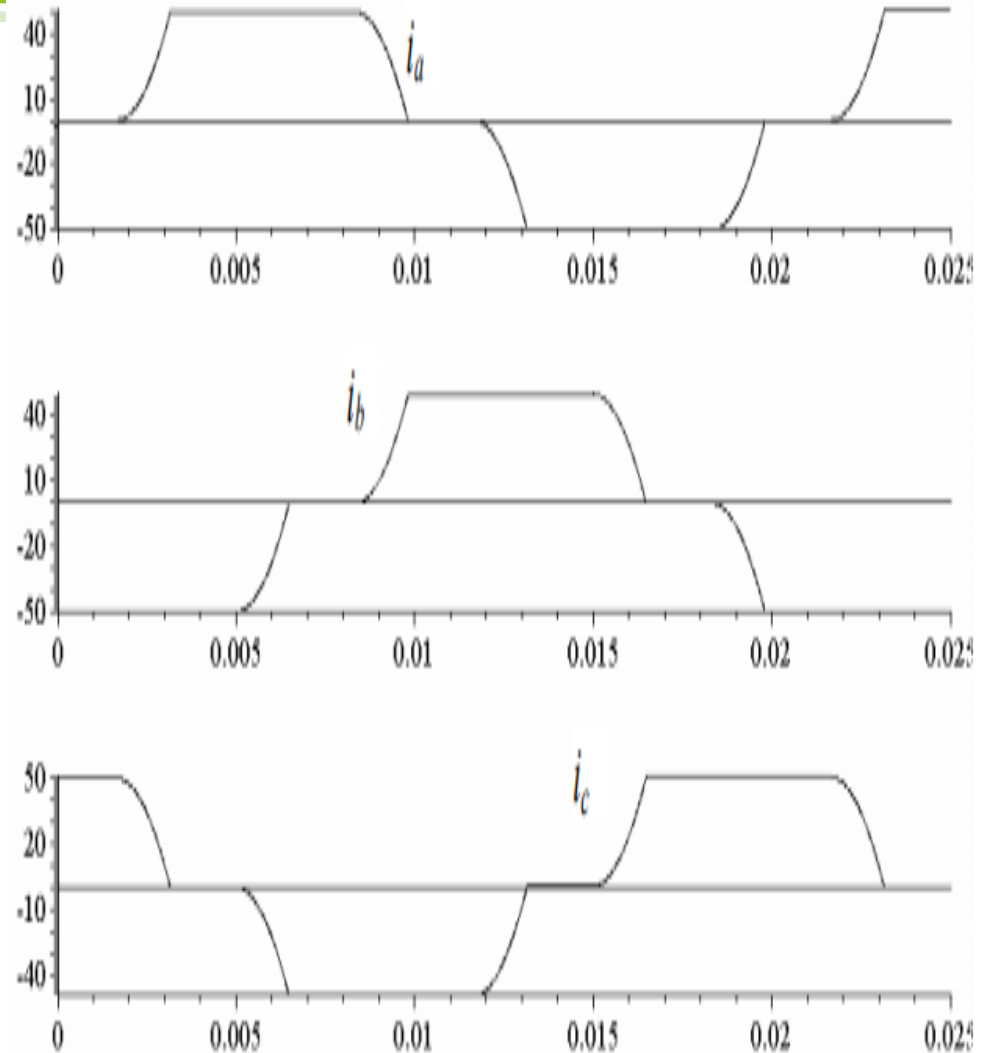
Operation

Currents waveforms

Half-wave



Full-wave



Analysis: Half-wave rectifier

1- Supply voltages:

$$V_a(\omega t) = V_m \sin(\omega t), \quad V_b(\omega t) = V_m \sin(\omega t - 2\pi/3), \quad V_c(\omega t) = V_m \sin(\omega t - 4\pi/3)$$

2- Output Load voltage

During the overlap period $0:\mu$

$$v_{an} = L_s \frac{di_a}{dt} + v_o$$

$$v_{bn} = L_s \frac{di_b}{dt} + v_o$$

Assuming that I_d remains constant during the overlap time, so

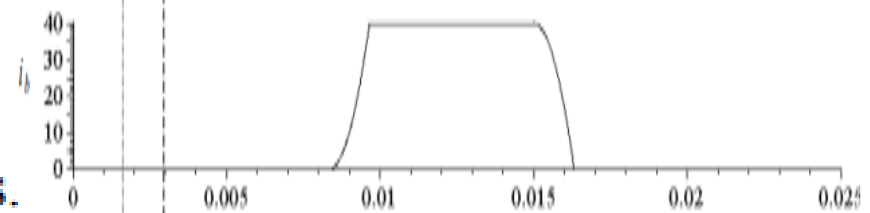
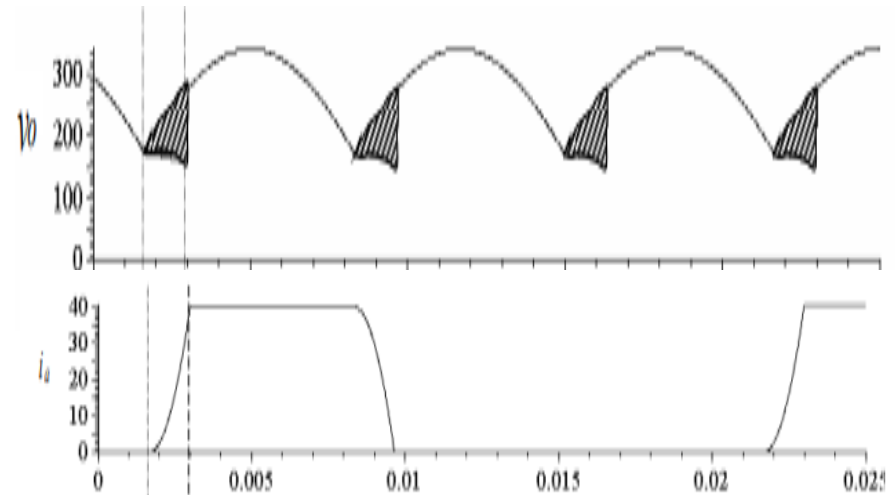
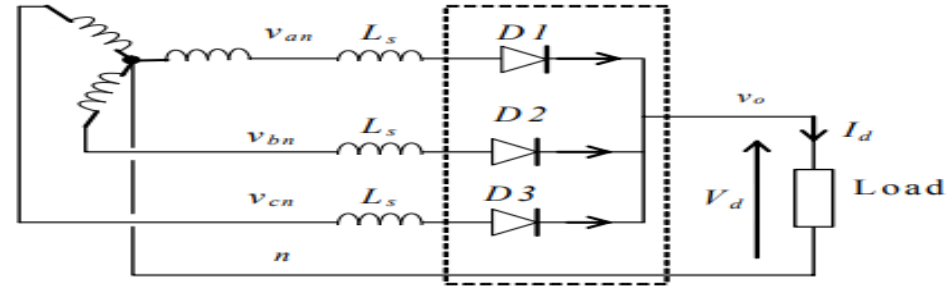
$$i_a + i_b = \bar{I}_d,$$

Differentiate both sides

$$\frac{di_a}{dt} = -\frac{di_b}{dt}$$

Adding the voltage equations and canceling the equal but opposite terms,

$$v_o = \frac{v_{an} + v_{bn}}{2}, \text{ during the overlap process.}$$



Analysis: Half-wave rectifier

$$V_a(\omega t) = V_m \sin(\omega t), \quad V_b(\omega t) = V_m \sin(\omega t - 2\pi/3), \quad V_c(\omega t) = V_m \sin(\omega t - 4\pi/3)$$

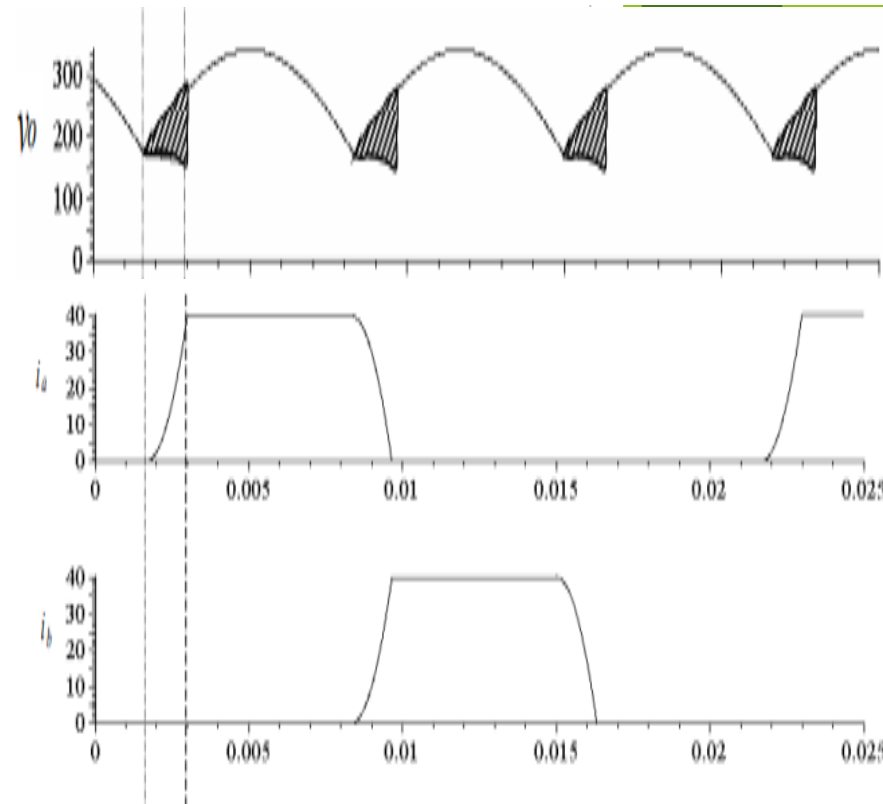
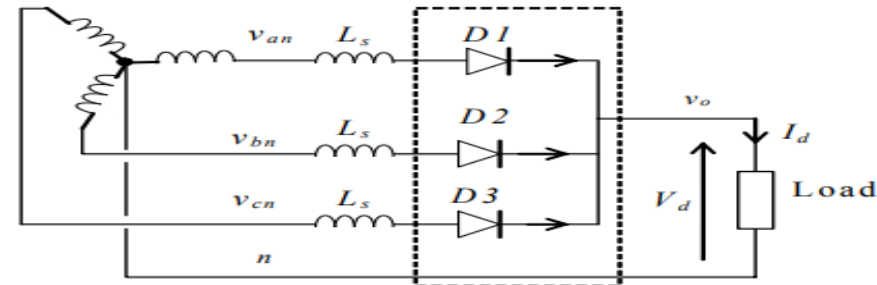
The part of the positive voltage pulse lost due to overlap starting from angle $\omega t = \pi/6$ is given by:

$$v_{bn} - \frac{v_{bn} + v_{an}}{2} = \frac{v_{bn} - v_{an}}{2} = L_s \frac{di}{dt}$$

The area (shaded) inside the voltage pulse lost due to overlap is given by:

$$\int_{\frac{\pi}{6}}^{\frac{\pi}{6} + \mu} \left(\frac{v_{bn} - v_{an}}{2} \right) d(\omega t) = \omega L_s \int_0^{I_d} di = \omega L_s I_d$$

Note that $(v_b - v_a)$ is the line-line voltage v_{ba} . The integral on the right hand side by shifting the origin by $\pi/6$ to the left. Thus



Analysis: Half-wave rectifier

$$V_a(\omega t) = V_m \sin(\omega t), \quad V_b(\omega t) = V_m \sin(\omega t - 2\pi/3), \quad V_c(\omega t) = V_m \sin(\omega t - 4\pi/3)$$

$$\int_0^\mu \frac{\sqrt{3} V_{max}}{2} \sin \omega t d(\omega t) = \omega L_s I_d$$

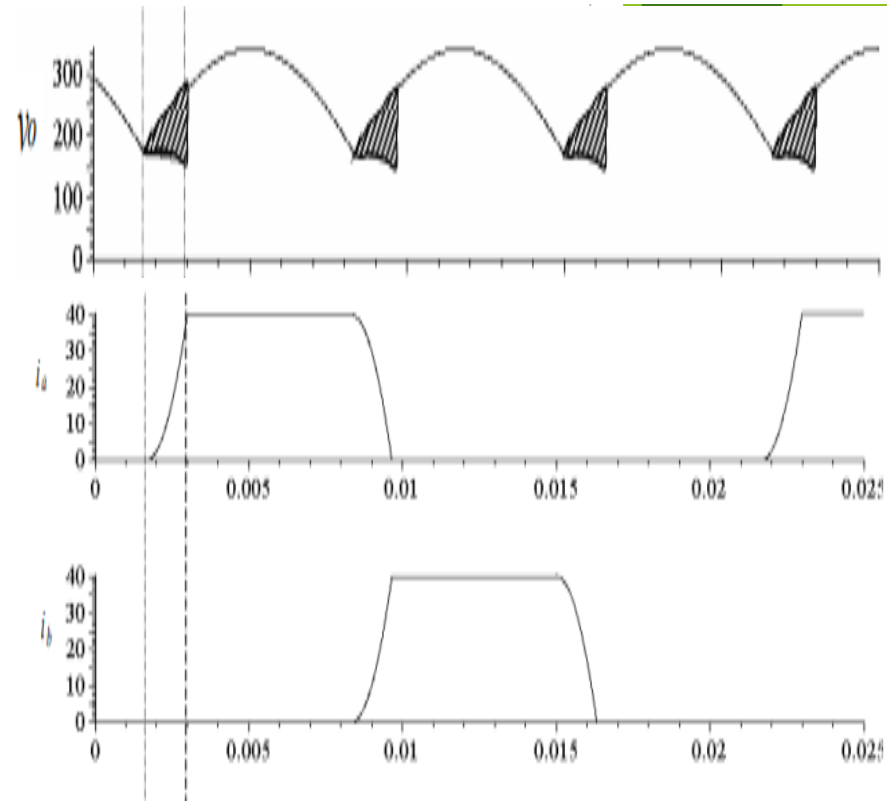
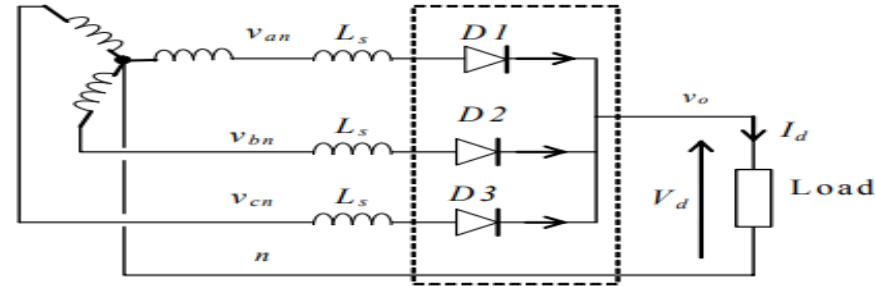
$$\therefore 1 - \cos \mu = \frac{2\omega L_s}{V_{max l-l}} I_d$$

where $V_{max l-l} = \sqrt{3} V_{max}$

$$\cos \mu = 1 - \frac{2\omega L_s}{V_{max l-l}} I_d$$

The dc output voltage

$$V_d = \frac{3\sqrt{3} V_{max}}{2\pi} \cdot \frac{3\omega L_s}{2\pi} I_d = \frac{3V_{max l-l}}{2\pi} \left(1 - \frac{\omega L_s}{V_{max l-l}} I_d \right)$$



Analysis: Half-wave Controlled rectifier

1- The Load voltage incase HWCR ☺ :

$$V_a(\omega t) = V_m \sin(\omega t), \quad V_b(\omega t) = V_m \sin(\omega t - 2\pi/3), \quad V_c(\omega t) = V_m \sin(\omega t - 4\pi/3)$$

$$\int_{\alpha}^{\alpha+\mu} \frac{\sqrt{3} V_{max}}{2} \sin \omega t d(\omega t) = \omega L_s I_d$$

$$\therefore 1 - \cos \mu = \frac{2\omega L_s}{V_{max} l-l} I_d$$

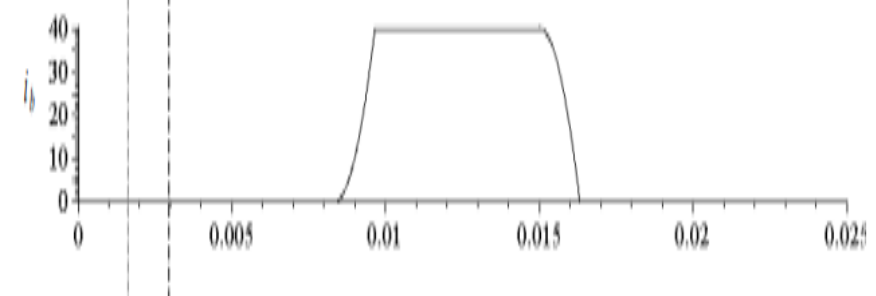
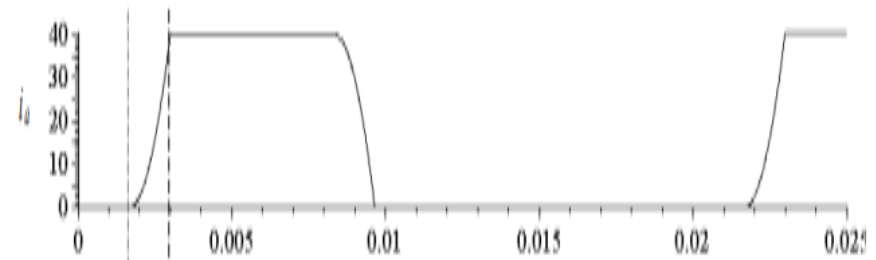
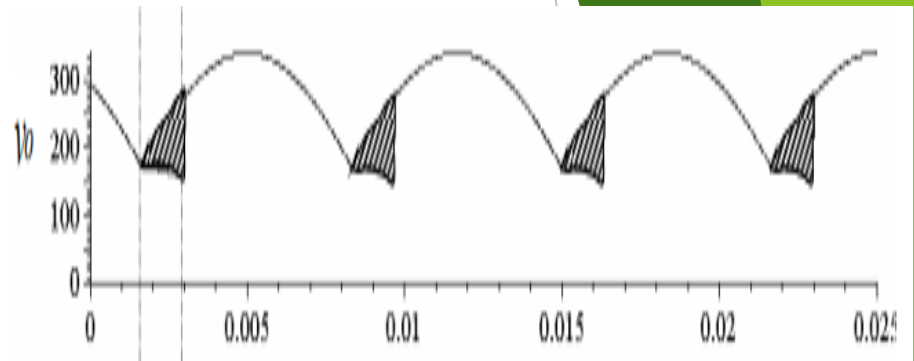
$$\cos(\alpha + \mu) = \cos(\alpha) - \frac{2\omega L_s}{V_{max} l-l} I_d$$

$$\mu = \alpha - \cos^{-1} \left(\cos(\alpha) - \frac{2\omega L_s}{V_{max} l-l} I_d \right)$$

The dc output voltage

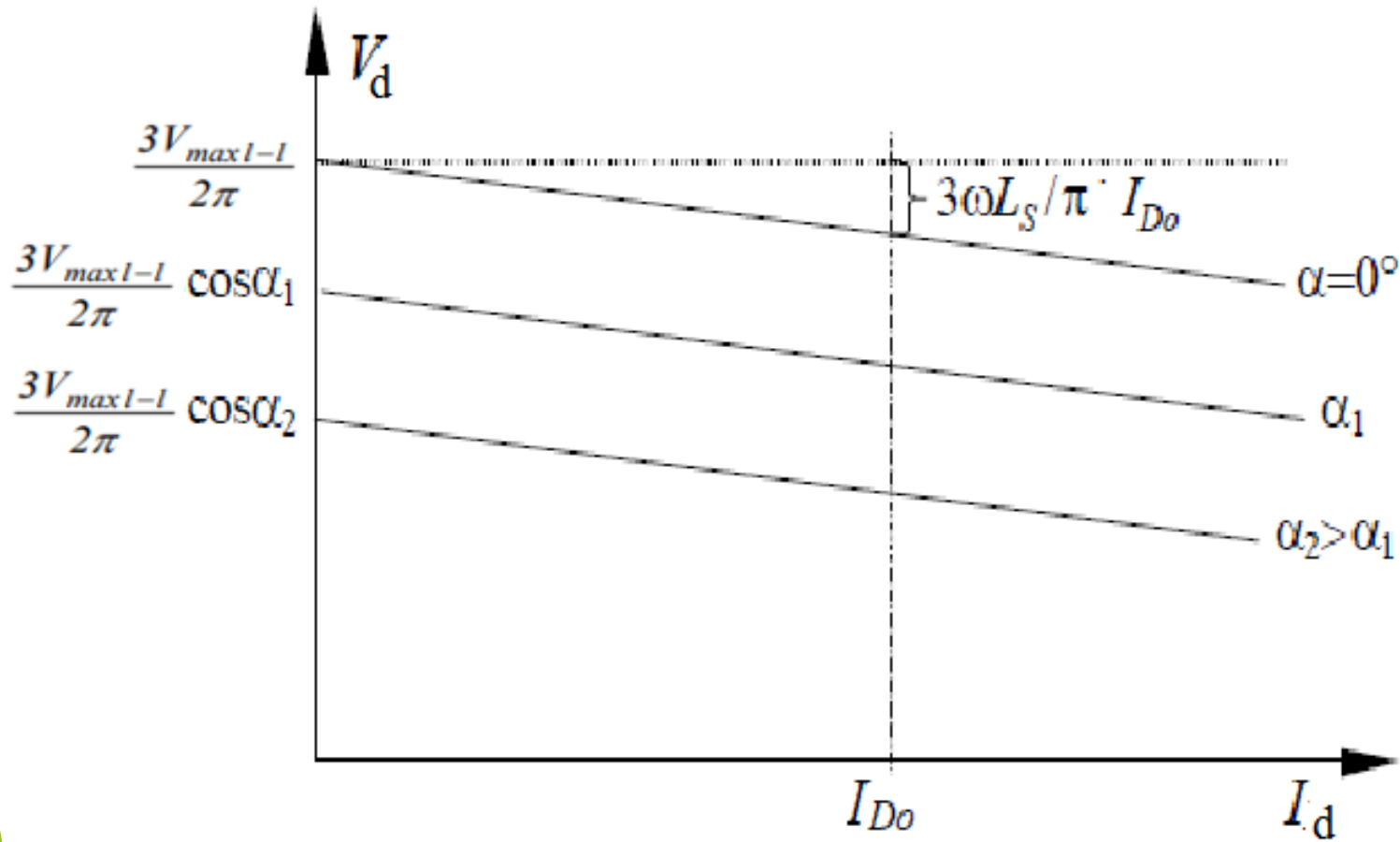
$$V_d = \frac{3\sqrt{3} V_{max}}{2\pi} - \frac{3\omega L_s}{2\pi} I_d = \frac{3V_{max} l-l}{2\pi} \left(1 - \frac{\omega L_s}{V_{max} l-l} I_d \right)$$

$$V_d = \frac{3 \cdot V_{ml}}{4 \cdot 2\pi} [\cos \alpha + \cos(\alpha + \mu)]$$



Analysis: Half-wave Controlled rectifier

Regulation characteristic of the rectifier



Analysis: Full-wave rectifier

1- Supply voltages:

$$V_a(\omega t) = V_m \sin(\omega t), \quad V_b(\omega t) = V_m \sin(\omega t - 2\pi/3), \quad V_c(\omega t) = V_m \sin(\omega t - 4\pi/3)$$

During the overlap period $0: \mu$

$$v_{an} = L_s \frac{di_a}{dt} + v_o$$

$$v_{bn} = L_s \frac{di_b}{dt} + v_o$$

when D_1 and D_3 are in overlap due to the source inductance L_s and where all voltages are with respect to the fictitious neutral point. v_o

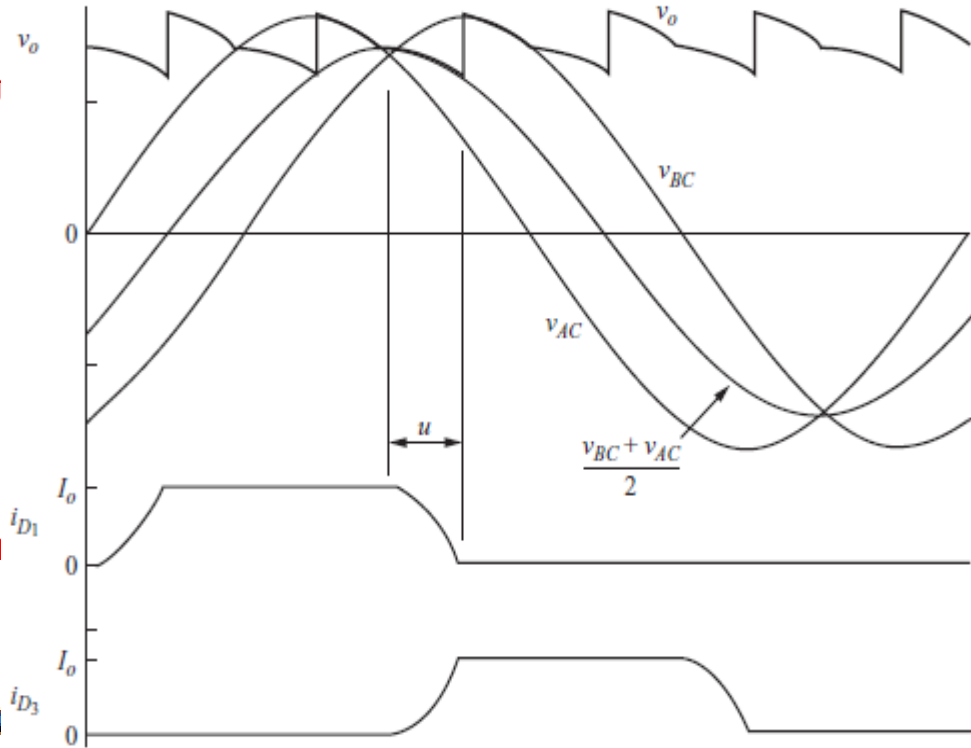
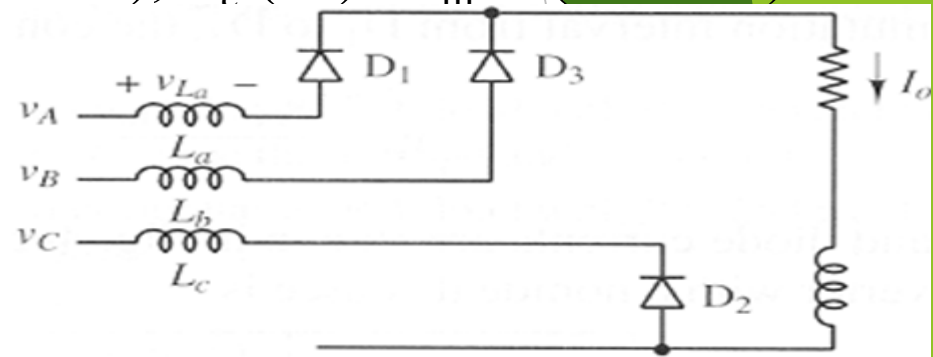
$$i_a + i_b = \bar{I}_d,$$

Differentiate both sides

$$\frac{di_a}{dt} = -\frac{di_b}{dt}$$

Adding the voltage equations and canceling the equal but opposite terms,

$$v_o = \frac{v_{an} + v_{bn}}{2}, \quad \text{during the overlap period}$$



(c)

Analysis: Full-wave rectifier

1- Supply voltages:

$$V_a(\omega t) = V_m \sin(\omega t), V_b(\omega t) = V_m \sin(\omega t - 2\pi/3), V_c(\omega t) = V_m \sin(\omega t - 4\pi/3)$$

During the overlap period $0 < \mu < \pi/6$

$$v_b - \frac{v_b + v_a}{2} = \frac{v_b - v_a}{2} = L_s \frac{di}{dt}$$

Integrating for the duration of the overlap

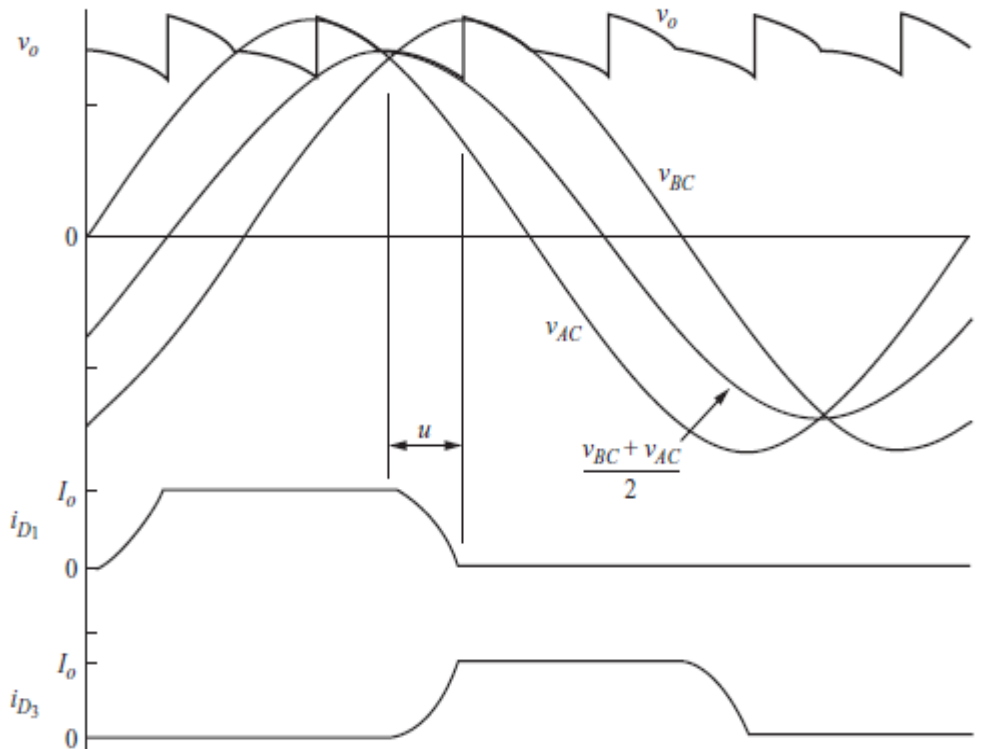
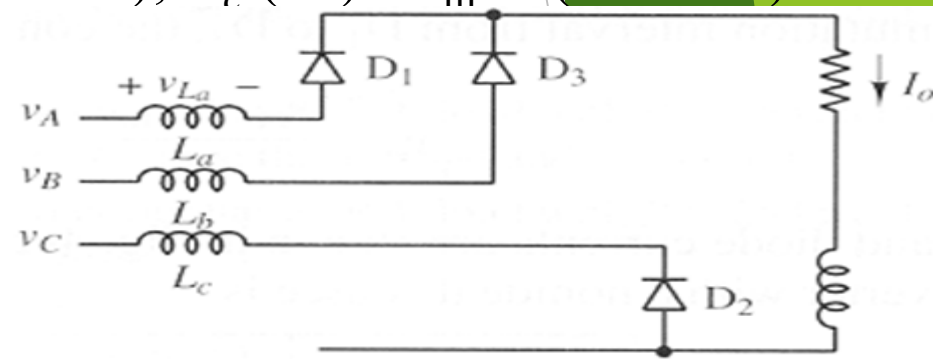
$$\int_{\pi/6}^{\pi/6 + \mu} \left(\frac{v_b - v_a}{2} \right) d(\omega t) = \omega L_s \int_0^{I_d} di$$

$$\int_0^{\mu} \frac{\sqrt{3} V_{max}}{2} \sin \omega t d(\omega t) = \omega L_s I_d$$

$$\therefore 1 - \cos \mu = \frac{2\omega L_s}{V_{max} l - l} I_d$$

$$\cos \mu = 1 - \frac{2\omega L_s}{V_{max} l - l} I_d$$

Compare with HWR



(c)

Analysis: Full-wave rectifier

1- Supply voltages:

$$V_a(\omega t) = V_m \sin(\omega t), \quad V_b(\omega t) = V_m \sin(\omega t - 2\pi/3), \quad V_c(\omega t) = V_m \sin(\omega t - 4\pi/3)$$

The dc output voltage V_d is given by

$$V_d = \frac{3V_{max} - I}{\pi} - \frac{I}{\pi/3} \int_0^{\mu} \frac{V_{max} - I}{2} \sin \omega t d(\omega t)$$

as

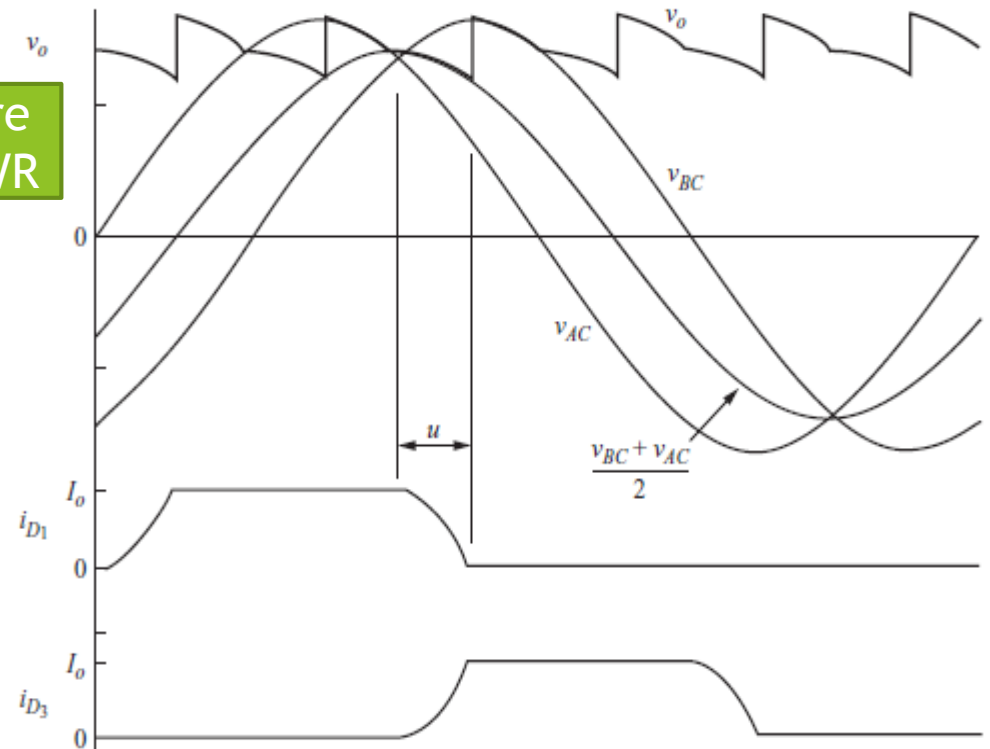
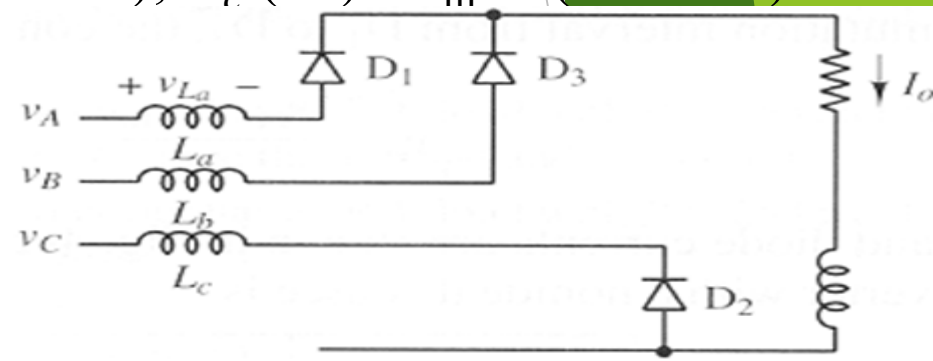
$$\int_0^{\mu} \frac{\sqrt{3}V_{max}}{2} \sin \omega t d(\omega t) = \omega L_s I_d$$

so

$$V_d = \frac{3V_{max} - I}{\pi} - \frac{3\omega L_s}{\pi} I_d$$

$$V_d = \frac{3V_{max} - I}{\pi} \left(1 - \frac{\omega L_s}{V_{max} - I} I_d \right)$$

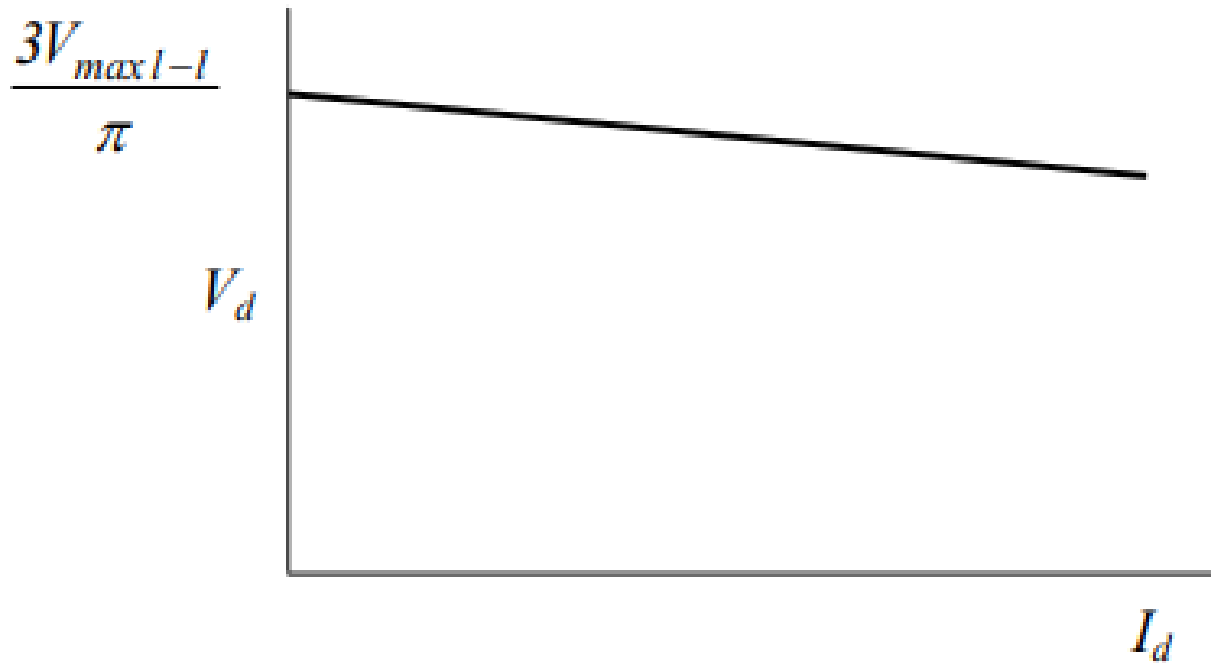
Compare with HWR



(c)

Analysis: Full-wave rectifier

Regulation characteristic of the rectifier



Questions

Q₁) what are the effect of source inductance on the load voltage?

Q₂) Deduce the average load voltage of three-phase full wave controlled rectifier with nonideal supply.

Q₃) What is the control range of α in the pervious case studies?